

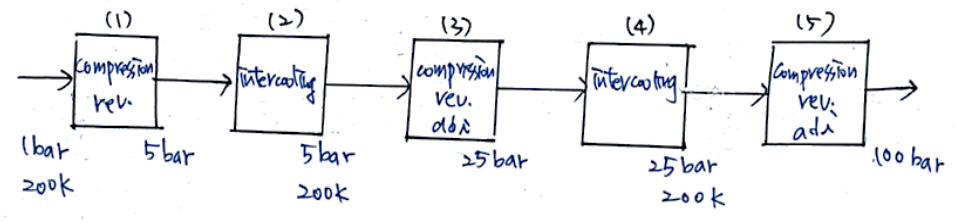
5.8 As in Illustration 5.1-1 it is desired to produce liquefied methane; however, the conditions are now changed so that the gas is initially available at 1 bar and 200 K, and methane leaving the cooler will be at 100 bar and 200 K. The flash drum is adiabatic and operates at 1 bar, and each compressor stage can be assumed to operate reversibly and adiabatically. A three-stage compressor will be used, with the first stage compressing the gas from 1 bar to 5 bar, the second stage from 5 bar to 25 bar, and the third stage from 25 bar to 100 bar. Between stages the gas will be isobarically cooled to 200 K.

- a. Calculate the amount of work required for each kilogram of methane that passes through the compressor in the simple liquefaction process.
- b. Calculate the fractions of vapor and liquid leaving the flash drum in the simple liquefaction process of Fig. 5.1-1 and the amount of compressor work required for each kilogram of LNG produced.
- c. Assuming that the recycled methane leaving the heat exchanger in the Linde process (Fig. 5.1-2) is at 1 bar and 200 K, calculate the amount of compressor work required per kilogram of LNG produced.

5.8

10

(a)



Take (1) as the system

Mass Balance

$$\frac{dM}{dt} \overset{0 \text{ s.s.}}{=} \dot{M}_{in} + \dot{M}_{out} \Rightarrow \dot{M}_{out} = -\dot{M}_{in}$$

Energy Balance

$$\frac{dU}{dt} = \dot{M}_{in} \hat{H}_{in} + \dot{M}_{out} \hat{H}_{out} + \dot{Q} + \dot{W}$$

$$\Rightarrow \dot{W} = \dot{M}_{in} (\hat{H}_{out} - \hat{H}_{in}) \Rightarrow \frac{\dot{W}}{\dot{M}_{in}} = \hat{H}_{out} - \hat{H}_{in}$$

Entropy Balance

$$\frac{dS}{dt} \overset{0 \text{ s.s.}}{=} \dot{M}_{in} \hat{S}_{in} + \dot{M}_{out} \hat{S}_{out} + \frac{\dot{Q}}{T} + \dot{S}_{gen}$$

$$\Rightarrow \hat{S}_{in} = \hat{S}_{out}$$

From Eq. 7.3-2: $\hat{H}_{in}(200\text{K}, 1\text{bar}) = 176.7 \text{ kJ/kg}$

$$\hat{S}_{in}(200\text{K}, 1\text{bar}) = 6.5 \text{ kJ/kg}\cdot\text{K} = \hat{S}_{out}$$

$$\Rightarrow \hat{H}_{out}(s = 6.5 \text{ kJ/kg}\cdot\text{K}, 5\text{bar}) = 963 \text{ kJ}$$

$$\Rightarrow \frac{\dot{W}}{\dot{M}_{in}} = 963 - 176.7 = 196 \text{ kJ/kg}$$

Take (2) as the system

$$\frac{\dot{W}_{in}}{\dot{M}_{in}} = \hat{H}_{out} - \hat{H}_{in} \quad \text{from Fig 3.3-2: } \hat{H}_{in}(200k, 5 \text{ bar}) = 760 \text{ kJ/kg.}$$

$$\hat{S}_{in}(200k, 5 \text{ bar}) = 5.65 \text{ kJ/kg.K}$$

$$\Rightarrow \hat{H}_{out}(s=5.65 \text{ kJ/kg.K}, 25 \text{ bar}) = 960 \text{ kJ/kg}$$

$$\Rightarrow \frac{\dot{W}_{in}}{\dot{M}_{in}} = 960 - 760 = 200 \text{ kJ/kg.}$$

Take (3) at the system

$$\frac{\dot{W}_{in}}{\dot{M}_{in}} = \hat{H}_{out} - \hat{H}_{in} \quad \text{from Fig 3.3-2: } \hat{H}_{in}(200k, 25 \text{ bar}) = 718 \text{ kJ/kg.}$$

$$\hat{S}_{in}(200k, 25 \text{ bar}) = 4.65 \text{ kJ/kg.K}$$

$$\Rightarrow \hat{H}_{out}(s=4.65 \text{ kJ/kg.K}, 100 \text{ bar}) = 855 \text{ kJ/kg}$$

$$\Rightarrow \frac{\dot{W}_{in}}{\dot{M}_{in}} = 855 - 718 = 137 \text{ kJ/kg}$$

The total work:

$$196 + 200 + 137 = 533 \text{ kJ/kg.}$$

(b) Take the value as the system. ③

From energy balance

$$\frac{dU}{dt} \overset{0 \text{ s.s.}}{=} \dot{M}_{in} \hat{H}_{in} + \dot{M}_{out} \hat{H}_{out} + \dot{Q} + \dot{W}$$

$\dot{W} \rightarrow$ no work.

$$\Rightarrow \hat{H}_{in} = \hat{H}_{out}$$

mass fraction of Liq.

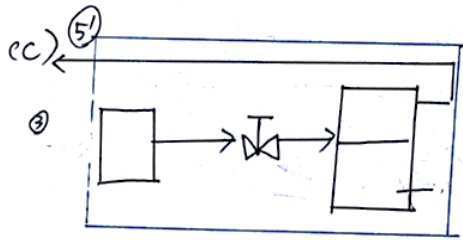
$$\text{Fig 3.3-2 } \hat{H}_{in}(200\text{K}, 100\text{ bar}) = (1-x) \hat{H}(\text{sat. Liq. } 1\text{ bar}) + x \hat{H}(\text{sat. vap. } 1\text{ bar})$$

$$\Rightarrow 423 = (1-x) \cdot 71 + x \cdot 582$$

↑ ↑ ↗
From Fig 3.3-2

$$\Rightarrow x = 0.689$$

$$\Rightarrow \frac{533}{(1-0.689)} = 1713 \text{ kJ of work are required for each kg. of LMG produced.}$$



From mass balance

$$\frac{dM}{dt} = \dot{M}_3 + \dot{M}_5' + \dot{M}_6 \Rightarrow \dot{M}_6 + \dot{M}_5' = -\dot{M}_3$$

From energy balance

$$\frac{dU}{dt} \overset{\text{SS.}}{=} \dot{M}_3 \hat{H}_3 + \dot{M}_5' \hat{H}_5' + \dot{M}_6 \hat{H}_6 + \overset{\text{adi}}{Q} + \overset{\text{no work.}}{W}$$

$$\Rightarrow \dot{M}_3 \hat{H}_3 + \dot{M}_5' \hat{H}_5' + \dot{M}_6 \hat{H}_6 = 0$$

$$\text{Let } \dot{M}_3 = 1 \quad \dot{M}_5' = -w \quad \dot{M}_6 = -1 + w$$

$$\hat{H}_3 (200\text{K}, 100\text{bar}) - w \hat{H}_5' (\text{sat. vap. } 1\text{bar}) + (-1+w) \hat{H}_6 (\text{sat. liq. } 1\text{bar}) = 0$$

$\downarrow \begin{matrix} 423 \\ \text{kJ/kg} \end{matrix}$
 $\downarrow \begin{matrix} 118 \\ \text{kJ/kg} \end{matrix}$
 $\downarrow \begin{matrix} 71 \\ \text{kJ/kg} \end{matrix}$

$$\Rightarrow w = 0.544 \quad 1-w = 0.456$$

$$\frac{5.33}{0.456} = 1168 \frac{\text{kJ}}{\text{kg}} \text{ \# of LNG produced.}$$